

WEEKLY TEST RANKER'S BATCH-02 TEST - 04 Balliwala **SOLUTION Date 06-10-2019**

[PHYSICS]

$$\eta = 1 - \frac{T_L}{T_H}$$

2.

3.
$$C_v$$
 for hydrogen = $\frac{5R}{2}$, C_0 for helium = $\frac{3R}{2}$

$$C_v$$
 for water vapour = $\frac{6R}{2}$

$$\therefore \quad \left[C_{v} \right]_{mix} = \frac{4 \times \frac{5R}{2} + 2 \times \frac{3R}{2} + 1 \times 3R}{4 + 2 + 1} = \frac{16R}{7}$$

$$C_p = C_v + R = \frac{16R}{7} + R = \frac{23R}{7}$$

As pressure is varrying linearly with volume, work done 4. dW = area under PV curve

$$= P_1(V_F - V_1) + \frac{1}{2}(P_F - P_1)(V_F - V_1)$$

$$=\frac{1}{2}(P_{F}+P_{I})(V_{F}-V_{I})$$

$$dU = \mu C_{_{\boldsymbol{V}}} dT = \mu \frac{R}{\gamma - 1} dT = \frac{P_{_{\boldsymbol{F}}} V_{_{\boldsymbol{F}}} - P_{_{\boldsymbol{I}}} V_{_{\boldsymbol{I}}}}{\gamma - 1}$$

$$\therefore dU = \frac{10^5 (8 \times 0.5) - 4 \times 0.2)}{(5/2) - 1} = 4.8 \times 10^5 J$$

5.
$$PV\gamma = constant$$

$$P_{\gamma}V^{\gamma-1}\gamma V + \Delta PV^{\gamma} = 0$$

$$\therefore \frac{\Delta P}{P} = -\gamma \frac{\Delta V}{V}$$

In cylinder A, heat is supplied at constant pressure while in cylinder B heat is supplied at constant volume.

$$(\Delta Q)_A = nC_p(\Delta T)_A$$

and $(\Delta Q)_B = nC_v(\Delta T)_B$
Given that :

$$(\Delta Q)_A = (\Delta Q)_B$$

$$\therefore$$
 $(\Delta T)_{B} = \frac{C_{p}}{C_{v}}(\Delta T)_{A} = (1.4)(30) = 42 \text{ K}$

Since, P-V graph of the process is a stright line and two points (V₀,2P₀) and (2V₀,P₀) are known, therefore 11. its equation will be,

$$(P - P_0) = \frac{(2P_0 - P_0)}{(V_0 - 2V_0)}(V - 2V_0) = \frac{P_0}{V_0}(2V_0 - V)$$

$$P = 3P_0 = \frac{P_0 V}{V_0}$$

According to equation for ideal gas,

$$T = \frac{PV}{nR}$$

$$= \left(3P_0 - \frac{P_0V}{V_0}\right) \frac{V}{nR}$$

$$= \frac{3P_0V_0V - P_0V^2}{nRV_0} \qquad(i)$$

For T to be maximum, $\frac{dT}{dV} = 0$

$$33P_0V_3 - 2P_0V = 0$$

or
$$V = \frac{3V_0}{2}$$

Putting this value in equation(i), we get,

$$T_{max} = \frac{3P_{o}V_{o}{\left(\frac{3V_{o}}{2}\right)} - P_{o}{\left(\frac{9}{4}V_{o}^{2}\right)}}{nRV_{o}} = \frac{9P_{o}V_{o}}{4nR}$$

12. In the curves 1-2 and 3-4, we find that the pressure is directly proportional to temperature. So, the volume remains unchanged, i.e., gas does not work.

.....(ii)

The work done during the isobaric processes 2-3 and 1-4 are as follows

$$W_{2-3} = P_2(V_3 - V_2)$$

Total work done =
$$P_2(V_3 - V_2) + P_1(_1V - V_4)$$

 $W_T = P_2V_3 - P_2V_2 + P_2V_2 - P_1V_4$
Three moles has been given, so

$$W = PV - PV + PV - PV$$

$$PV = nRT = 3RT$$

$$W_{T} = 3RT_{3} - 3RT_{2} + 3RT_{1} - 3RT_{4}$$

$$= 3R[T_{1} + T_{3} - T_{2} - T_{4}]$$

$$= 3R[400 + 2400 - 800 - 1200]$$

$$= 3R[I_1 + I_3 - I_2 - I_4]$$

$$= 3R[400 + 2400 - 800 - 1200]$$

$$= 3R \times 800 = 20 \times 10^3 J = 20 kJ$$

According to first law of thermodynamics: 13.

$$\Delta Q = \Delta U + \Delta W$$

For the process abc, $80 = \Delta U + 60$

or
$$\Delta U = 20 \text{ cal}$$

Since, ΔU is independent of path the internal energy change is same for both the paths abc and adc.

For the process adc, $\Delta Q = \Delta U + \Delta W$

$$\therefore \Delta W = \Delta Q - \Delta U = 30 - 20 = 10 \text{ cal}$$

- 14.
- 15. In adiabatic expansion we know that dQ = 0

$$dQ = dU + PdV \text{ or } 0 = dU + PdV$$

$$PdV = -dU$$

Thus, work done decrease internal energy which is function of temperature. Hence, temperature also decreases.

16. For mixture of gases, let specific heat be C,

$$\boldsymbol{C}_{v} = \frac{n_{1}(\boldsymbol{C}_{v})_{1} + n_{2}(\boldsymbol{C}_{v})_{2}}{n_{1} + n_{2}}$$

where
$$(C_v)_1 = \frac{5R}{2}, (C_v)_2 = \frac{3R}{2}$$

$$\therefore C_{v} = \frac{2 \times \frac{5R}{2} + 8 \times \frac{3R}{2}}{2 + 8} = \frac{17R}{10} = 1.7R$$

17. Two chambers are kept separate at (P, 5V) and (10P, V). When the piston is allowed to move, the gases are kept separated but the pressure has to be equal

Let the equal new pressure on the both sides of piston in its equilibrium position be P'.

As the process is isothermal, hence

for LHS portion:
$$P(5V) = P'(5V - x)$$

and for RHS portion :
$$10P(V) = P'(V + x)$$

solving equations (i) and (ii) we get;

$$x = 3V$$

:. New volume of LHS portion = 2V and new volume of RHS portion = 4V

18. PV^{γ} = constant for an adiabatic process

Given: $P^3 \times V^4 = constant$

or
$$PV^{4/3} = constant$$

$$\left(\text{as P}^3 \propto \frac{1}{V^4}\right)$$

or
$$\gamma = \frac{4}{3} = 1.33$$

20. From first law of thermodynamics,

$$Q = \Delta U + W$$

For path iaf,
$$50 = \Delta U + 20$$

$$\therefore \Delta U = U_i - U_i = 30 \text{ cal}$$

For path ibf,
$$Q = \Delta U + W$$

or
$$W = Q - \Delta U$$

$$= 36 - 30 = 6$$
 cal

21. In cyclic process, the amount of heat given to system is equal to the net work done by the system.

Hence, correct answer is (b)

22. Work done in complete cycle

$$= P_0 V_0$$

Heat given to the gas in going from A to B

$$nC_v g \Delta T = n.\frac{3}{2} R \Delta T$$

Heat given to the gas in going from B to C

$$= nC_v \Delta T = n \left(\frac{5}{2}R\right) \Delta T$$

$$=\frac{5}{2}(2P_0)\Delta T = 5P_0V_0$$

Heat is rejected in going from C to D and then D to A.

Effeciency,
$$\eta = \frac{\text{Work done by the gas}}{\text{Heat given to the gas}} \times 100$$

$$=\frac{P_0V_0\times100}{\frac{3}{2}P_0V_0+5P_0V_0}=\frac{2\times100}{13}=15.4\%$$

23.
$$\frac{K_{Fe}A(100-\theta)}{d} = \frac{K_{Ag}(\theta-0)}{d}$$

$$\frac{K_{Fe}}{K_{Ag}} = \frac{\theta}{100 - \theta} \text{ or } \frac{1}{11} = \frac{\theta}{100 - \theta}$$

$$\theta = \frac{100}{12} = 8.3^{\circ}C$$

24.
$$\frac{dQ}{dt} = \frac{dQ_1}{dt} + \frac{dQ_2}{dt}$$

$$\frac{K(A_1+A_2)(\theta_1-\theta_2)}{d} = \frac{K_1A_1(\theta_1-\theta_2)}{d} + \frac{K_2A_2(\theta_1-\theta_2)}{d}$$

$$\therefore K = \frac{K_1 A_1 + K_2 A_2}{A_1 + A_2}$$

25. 26. Equivalent electrical circuit, will be as shown in figure.

Temperature difference between A and D is 180°C, which is equally distributed in all the rods. Therefore, temperature difference between A and B will be 60°C, or temperature of B should be 140°C

27.

Rate of flow of heat $\frac{dQ}{dt}$ or H is equal throughout the rod. Temperature difference is given by: 28.

or
$$R.D \propto$$
 Thermal Resistance R

Where,
$$R = \frac{1}{KA}$$
 or $R \propto \frac{1}{A}$

Area across CD is less. Therefore, T.D. cross CD will be more.

29. Here,
$$K_1 = K_2$$
, $I_1 = I_2 = 1$ m

Here,
$$K_1 = K_2$$
, $I_1 = I_2 = 1$ m,
 $A_1 = 2A$, $A_2 = A$
 $T_1 = 100$ °C, $T_2 = 70$ °C

$$\frac{\Delta Q}{\Delta t} = \frac{K2A(100 - T)}{1} = \frac{KA(T - 70)}{1}$$

or
$$T = 90^{\circ}$$

30. We know that :
$$\frac{dQ}{dt} = KA \frac{d\theta}{dx}$$

In steady state flow of heat,

$$d\theta = \frac{dQ}{dt}.\frac{1}{KA}dx$$

or
$$\theta_{H} - \theta = K'x$$

or
$$\theta = \theta ... - K'x$$

Equation, $\theta = \theta_{\perp} - K'x$ represents a straight line.

31.

32.

33. For parallel combination of two rods of equal length and equal area of cross-section:

$$K = \frac{K_1 + K_2}{2} = \frac{K_1 + \frac{4K_1}{3}}{2} = \frac{7K_1}{6}$$

Hence,
$$\frac{K}{K_1} = \frac{7}{6}$$

When a body cools by radiation, according to Stefan's law, 34.

$$\frac{dT}{dt}\frac{eA\sigma}{mc}\Big(T^4-T_0^4\,\Big)$$

Here, m, c, e, T and T_0 are same for all bodies; so

$$\frac{dT}{dt} \propto area A$$

Now, as for a given mass, area of the sphere is minimum, hence it will have the lowest rate of cooling.

35. Radius of small sphere = r and thicknes = t Radius of bigger sphere = 2r and thickness = t/4

Mass of ice melted = $\frac{4}{3}\pi r^3 p$

For bigger sphere :
$$\frac{K_1 4\pi (2r^2) \times 100}{t/4} = \frac{\frac{4}{3}\pi (2r^2)\rho L}{25 \times 60}$$

For smaller sphere :
$$\frac{K_2 4\pi r^2 \times 100}{t} = \frac{\frac{4}{3}\pi r^2 \rho L}{16 \times 60}$$

$$\frac{K_1}{K_2} = \frac{8}{25}$$

36. According to Wein's law

$$\lambda_m T = constant$$

or
$$(\lambda_m)_1 T_1 = (\lambda_m)_2 T_2$$

$$\lambda_{\rm m} T = {\rm constant}$$

or $(\lambda_{\rm m})_1 T_1 = (\lambda_{\rm m})_2 T_2$
or $11 \times 10^{-5} \times T_1 = (5.5 \times 10^{-5}) \times T_2$

$$T_1 = \frac{1}{2}T_2$$

37.
$$P \propto \frac{T^4}{d^2}$$

When T and d are doubled, then power received by the surface

$$P^{+} \propto \frac{\left(2T\right)^4}{\left(2d\right)^2} \propto \frac{2^4 \, T^4}{2^2 d^2} \propto \frac{4T^4}{d^2}$$

Hence,
$$P' = 4P$$

38.

39.

40.

41.

12. According to Newton's law of cooling, rate of loss of heat $\infty(T-T_0)$ where T is the average temperature in the given time internal. Hence,

 $\frac{Q}{t} \propto K$ or Kt = constant43.

$$\therefore \quad \frac{K_1}{K_2} = \frac{t_2}{t_1} = \frac{40}{20} = \frac{2}{1}$$

44. For slabs in series, we have,

$$R_{eq.} = R_1 + R_2$$

i.e.,
$$\frac{5x}{K_{eq.}A} = \frac{4x}{2KA} + \frac{x}{KA}$$

Now, is steady state, rate of heat transfer through the slab

$$\frac{K_{eq.}A(T_2-T_1)}{5x} = \left(\frac{5(T_2-T_1)K}{x}\right)f$$

Putting the value of K_{eq} , we get;

$$f = \frac{1}{3}$$

 $\frac{Q}{At} = \frac{K(\theta_1 - \theta_2)}{d} = constant$ 45.

$$\therefore K_{A}\left(\frac{\theta_{1}-\theta}{d}\right) = K_{B}\left(\frac{\theta-\theta_{2}}{d}\right)$$

$$\frac{K_{_{A}}}{K_{_{B}}} = \frac{\theta - \theta_{_{2}}}{\theta_{_{1}} - \theta} \text{ or } 3 = \frac{\theta - \theta_{_{2}}}{\theta_{_{1}} - \theta}$$

or
$$3\theta_1 - \theta_2 = 4\theta$$
(i)
Given $\theta_1 - \theta_2 = 20^{\circ}$ C(ii)
Solving eqns. (i) & (ii), we have $\theta - \theta_2 = 15^{\circ}$ C

$$\begin{array}{ll} \therefore & q - q = \theta_1 - \theta_2 + \theta_2 - \theta \\ & = (\theta_1 - \theta_2) - (\theta - \theta_2) \\ & = 20^{\circ}\text{C} - 15^{\circ}\text{C} = 5^{\circ}\text{C} \end{array}$$